

Mathematical Theory of Non-Newtonian Fluid

1. Derivation of the Incompressible Fluid Dynamics
2. Existence of Non-Newtonian Flow and its Dynamics
3. Existence in the Domain with Boundary

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Drivation of the Incompressible Fluid Equations

1. Introduction
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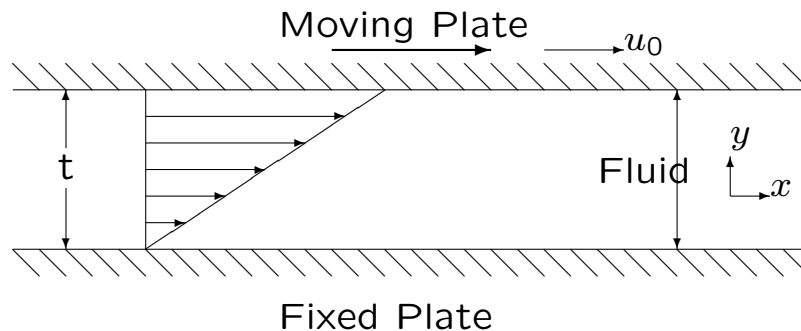
Introduction

Fluids: liquids and gases

A solid can resist an applied shear force and remain at rest, while a fluid cannot.

Newtonian Fluid : water, air

Non-Newtonian Fluid: grease, polymer, biological fluid



Velocity distribution between two parallel plate

Properties of Fluids:

1. Kinematic property
 - linear **velocity**, angular velocity, vorticity, acceleration, and strain rate
2. Transport property
 - **viscosity**, thermal conductivity, mass diffusivity
3. Thermodynamic property
 - **pressure**, thermal conductivity, temperature, enthalpy, entropy, specific heat
4. Other miscellaneous property
 - surface tension, vapor pressure

Kinematic Property:

- Lagrangean description : the scheme of following the trajectories of individual particles
- Eulerian description : the scheme describing the flow at fixed point as a function of time

Eulerian velocity vector fields

$$\begin{aligned}\mathbf{u}(\mathbf{x}, t) &= \mathbf{u}(x_1, x_2, x_3, t) \\ &= (u_1(x_1, x_2, x_3, t), u_2(x_1, x_2, x_3, t), u_3(x_1, x_2, x_3, t))\end{aligned}$$

Three fundamental law of mechanics :

Conservation of **mass**, **momentum**, energy in Lagrangean sense

[Relationship of Lagrangean and Eulerian Coordinates]

Let Q be any property

$$dQ = \frac{\partial Q}{\partial x_1} dx_1 + \frac{\partial Q}{\partial x_2} dx_2 + \frac{\partial Q}{\partial x_3} dx_3 + \frac{\partial Q}{\partial t} dt.$$

Since

$$dx_1 = u_1 dt, \quad dx_2 = u_2 dt, \quad dx_3 = u_3 dt,$$

we have

$$\begin{aligned} \frac{dQ}{dt} &= \frac{\partial Q}{\partial t} + u_1 \frac{\partial Q}{\partial x_1} + u_2 \frac{\partial Q}{\partial x_2} + u_3 \frac{\partial Q}{\partial x_3} \\ &= \frac{\partial Q}{\partial t} + (\mathbf{u} \cdot \nabla) Q \end{aligned}$$

$$\begin{cases} \frac{DQ}{Dt} = \frac{dQ}{dt} & \text{-- material derivative} \\ (\mathbf{u} \cdot \nabla) Q & \text{-- convective derivative} \\ \frac{\partial Q}{\partial t} & \text{-- local derivative} \end{cases}$$

[Reynolds' Transport Theorem]

For a control volume,

$$\begin{aligned} & \frac{D}{Dt} \int_{V(t)} Q(t) dV \\ &= \lim_{\delta t \rightarrow 0} \left\{ \frac{1}{\delta t} \left[\int_{V(t+\delta t)} Q(t+\delta t) dV - \int_{V(t)} Q(t) dV \right] \right\} \\ &= \lim_{\delta t \rightarrow 0} \left\{ \frac{1}{\delta t} \left[\int_{V(t+\delta t) - V(t)} Q(t+\delta t) dV \right] \right\} + \int_{\partial V(t)} \frac{\partial Q(t)}{\partial t} dV \\ &= \lim_{\delta t \rightarrow 0} \int_{\partial V(t)} Q(t+\delta t) \mathbf{u} \cdot n dS + \int_{V(t)} \frac{\partial Q}{\partial t} dV \\ &= \int_{\partial V(t)} Q(t) \mathbf{u} \cdot n dS + \int_{V(t)} \frac{\partial Q}{\partial t} dV \\ &= \int_{V(t)} \left[\nabla \cdot (Q\mathbf{u}) + \frac{\partial Q}{\partial t} \right] dV. \end{aligned}$$

Motion of Fluid particle:

- translation – $\mathbf{u}(\mathbf{x}, t)$
- rotation – $\frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} - \frac{\partial u_j}{\partial x_i} \right)$
- deformation

1. dilation : expansion or reduction of volume

$$\frac{\partial u}{\partial x}, \quad \frac{\partial v}{\partial y}, \quad \frac{\partial w}{\partial z}$$

2. shear strain : distortion

– the average decrease of the angle between two lines which are initially perpendicular in the unstrained state

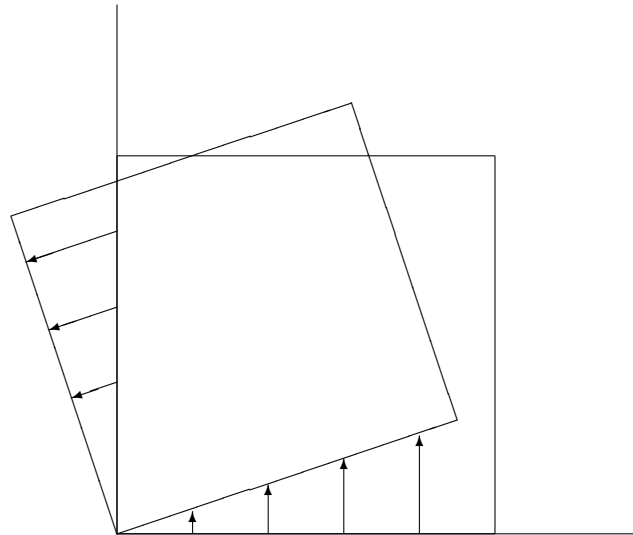
$$\frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

Notice that

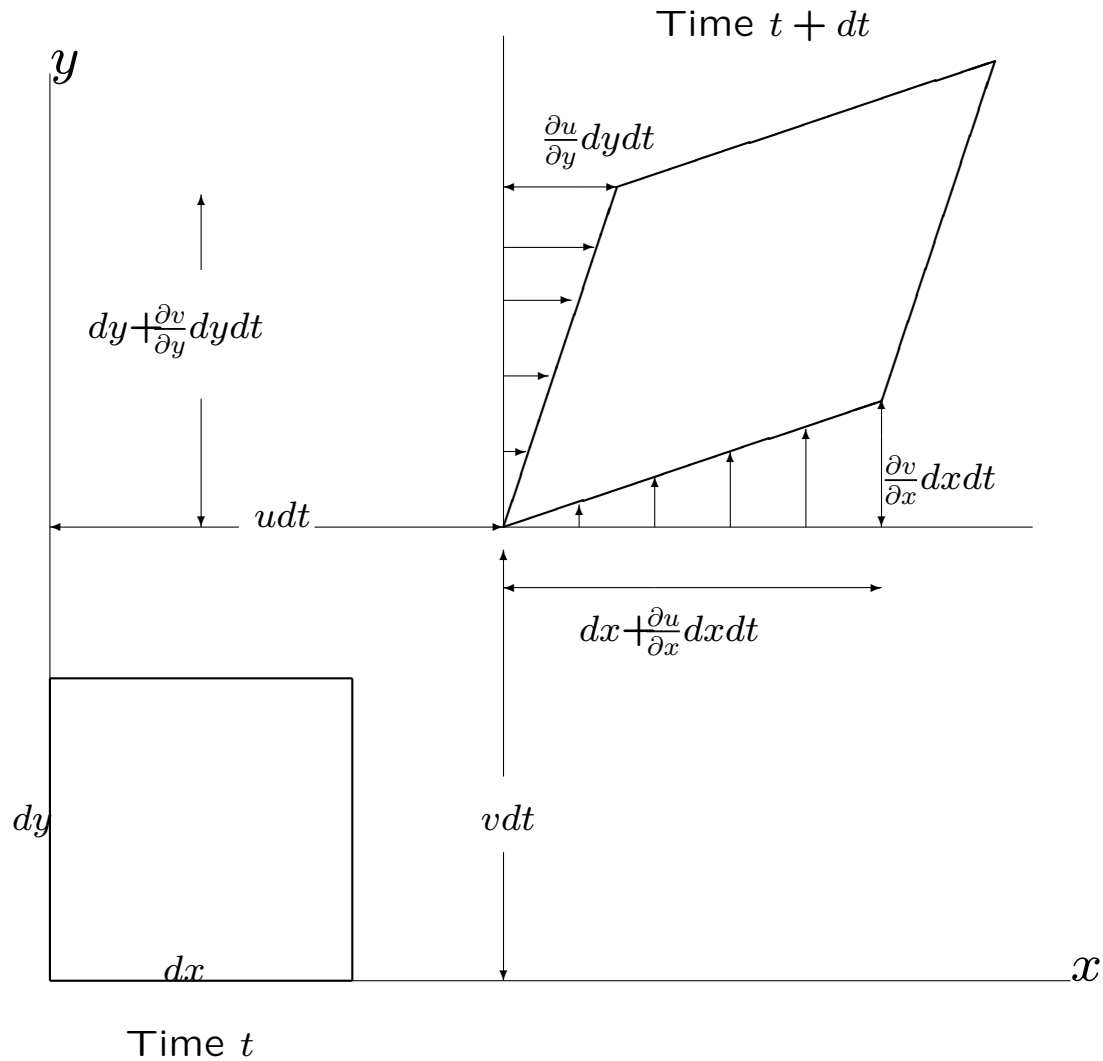
$$u_{i,j} = \frac{1}{2}(u_{i,j} + u_{j,i}) + \frac{1}{2}(u_{i,j} - u_{j,i}).$$

Means : each velocity derivative can be resolved into a **strain rate** plus an **angular velocity**

Rotation :

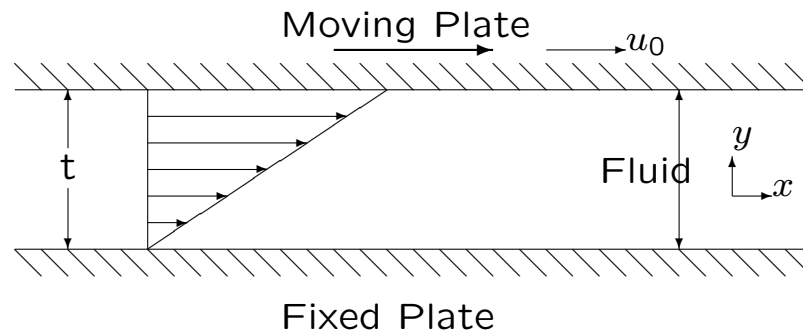


Distortion of a moving fluid element:



Transport property :

Viscosity : the property of a fluid which relates applied **stress** to the resulting **straining rate**



By the viscosity property of a fluid, if the upper plate move with speed V , then the fluid on the plate move with the same speed V .

Since there is no movement on fixed plate, the fluid on the ground doe not move.

$$[\text{Shear strain} = \epsilon_{ij}] = \frac{1}{2} \left(\frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \right) = \frac{1}{2} \frac{du}{dy} = \tau_{xy}$$

In general, shear stress τ_{ij} is a function of the strain rate ϵ_{ij} :

$$\tau_{ij} = f(\epsilon_{ij})$$

- If the relation is linear, it is Newtonian;

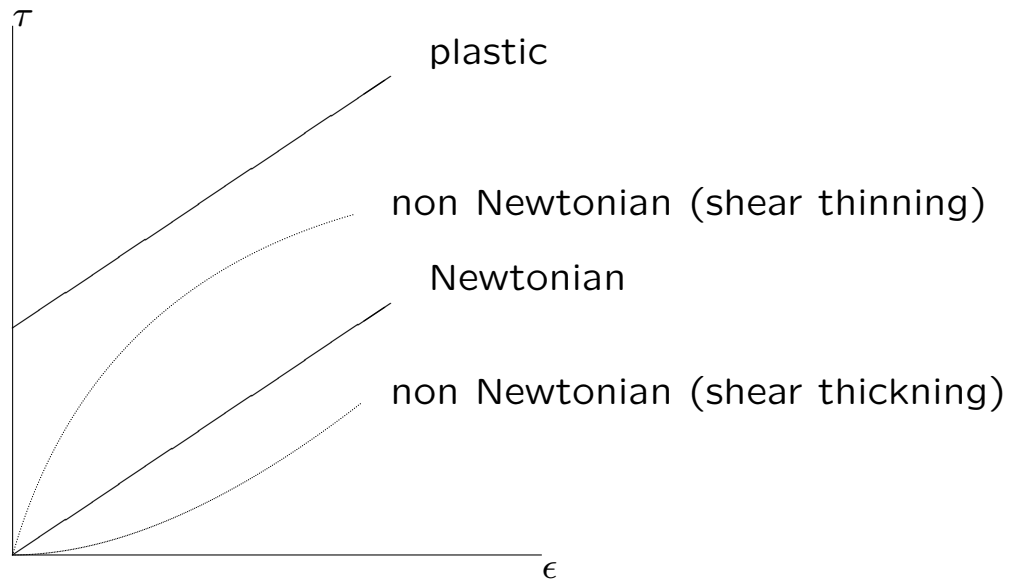
$$\tau_{ij} = \mu \frac{\partial u}{\partial y}.$$

The constant μ is the **viscosity**.

- If not, it is non-Newtonian.

$$\tau_{xy} = K \epsilon_{xy}^r$$

- τ_{xy} : shear stress,
- $\frac{\partial u}{\partial y}$: rate of strain
- μ : viscosity



Navier-Stokes equation

1. Conservation of Mass : Equation of Continuity

$$\begin{aligned} 0 &= \frac{D}{Dt} \int_V \rho dV \\ &= \int_V \left[\frac{\partial \rho}{\partial t} + \frac{\partial}{\partial x_k} (\rho u_k) \right] dV \\ &\quad \Leftarrow \text{Reynold's transport theorem} \end{aligned}$$

ρ : density

Therefore,

$$0 = \frac{\partial \rho}{\partial t} + \text{div}(\rho \mathbf{u}) = \frac{D\rho}{Dt} + \rho \text{div} \mathbf{u}.$$

If $\text{div} \mathbf{u} = 0$, then the fluid is called **incompressible**.

2. Conservation of Momentum ($\mathbf{F}=\mathbf{ma}$):

$$\frac{D\mathbf{u}}{Dt} = \frac{\partial\mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla)\mathbf{u}$$

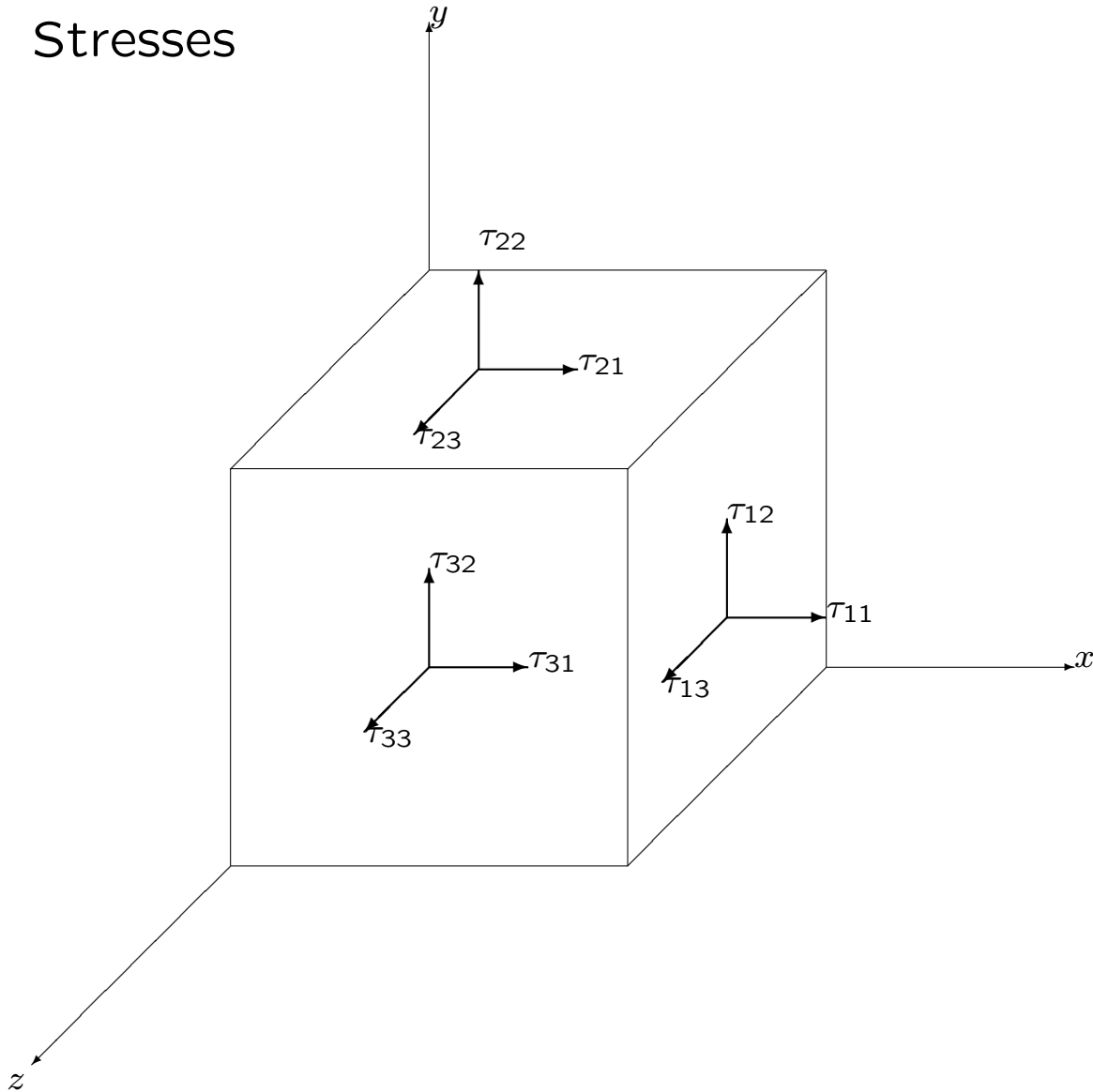
$$\begin{aligned}\frac{D}{Dt} \int_V \rho \mathbf{u} dV &= [\text{total force}] \\ &= [\text{body force}] + [\text{surface (exterior) force}] \\ &= \int_V \rho F_i dV + \int_S \tau_{ij} n_j dS \\ &= \int_V \left(\rho F_i + \frac{\partial \tau_{ij}}{\partial x_j} \right) dV \quad \Leftarrow [\text{divergence theorem}]\end{aligned}$$

\Rightarrow

$$\rho \frac{Du_i}{Dt} = \rho F_i + \frac{\partial \tau_{ij}}{\partial x_j}$$

- Body force $F_i = g \iff$ external fields such as gravity or electromagnetic potential
- Surface force $\text{div}\tau \iff$ external stress on the sides of the particle

Stresses



τ_{ij} : stress in the j direction on a face normal to the i axis

[Relation of force and deformation]

- fluid at rest :

$$\tau_{ij} = -\rho\delta_{ij}$$

$$-p = \tau_{xx} = \tau_{yy} = \tau_{zz} : \text{normal stress} = \text{pressure}$$

- fluid in motion:

- Newtonian fluid: linear relation of τ_{ij} and deformation rate

$$\tau_{ij} = -p\delta_{ij} + \mu\left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i}\right) + \delta_{ij}\lambda\text{div}\mathbf{u}$$

- Newtonian fluid: non-linear relation of τ_{ij} and deformation rate

Navier-Stokes Equations: Incompressible and Newtonian Fluid

$$\rho \frac{D\mathbf{u}}{Dt} = \rho \mathbf{g} - \nabla p + \mu \nabla^2 \mathbf{u}$$

\implies

$$\begin{cases} \frac{du_i}{dt} - \nu \Delta u_i + (u \cdot \nabla) u_i + \nabla_i p = f_i, \\ \nabla \cdot u = 0 \end{cases}$$

- Leray, 1934 Hopf, 1951
Existence of Weak Solutions
- 2D N-S: Uniqueness and Regularity

$$u \in L^\infty(0, \infty; H^1) \cap L^2(0, \infty; H^2)$$

- 3D N-S: Short Time Regularity

$$u \in L^\infty(0, T; H^1) \cap L^2(0, T; H^2)$$

- 3D N-S: Small Data, or Large Viscosity
 \implies Global Regularity
- 3D N-S: Regularity and Uniqueness :
quad Open Problem

Regularity

- Serrin, 1962

$$L^{r,r'}, \quad \frac{3}{r} + \frac{2}{r'} < 1.$$

- Caffarelli, Kohn & Nirenberg, 1982
- Constantin & Fefferman
- Choe, 1996 : Boundary L^∞ Regularity

Regularity Theorem for Navier-Stokes Equations[Bae and Choe, 1996, 2007]

Suppose that (u, p) is a weak solution. Let $u = (u_1, u_2, u_3)$. If $u_1, u_2 \in L_{loc}^{\infty, \infty}(Q)$, then

$$u_3 \in L_{loc}^{\infty, \infty}(Q).$$

Therefore, u is smooth.

Our Plan

- Use $\int \int |u|^3 dx dt \leq C$
- Show $\sup \int |u|^3 dx \leq C$
- Show $\int \int_{loc} |u| |\nabla u|^2 dx dt \leq C$
- Show $u \in L^{5,5}$
- Use Struwe's Regularity: If $u \in L^{5,5}$ Then u regular

Existence and Regularity Theorem for Non-Newtonian Fluids[Bae and Choe, 1997]

$$\left\{ \begin{array}{l} \frac{du_i}{dt} - \nu_1 \Delta u_i - \nu_2 \frac{\partial |e_{ij}|^r \epsilon_{ij}}{\partial x_j} + (u \cdot \nabla) u_i + \nabla_i p = f_i, \\ \nabla \cdot u = 0 \\ \epsilon_{ij} = \frac{1}{2} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \end{array} \right.$$

Then there is a weak solution for $r > -1$.

For $r > 2/5$ the solution is regular.